## Set of Components/Component Safety Data (acc. IEC 61508)

Set of Components/Component	Lined Butterfly Valves Series XLD	
Manufacturer	XOMOX International GmbH & Co.OHG	
Component Type	Туре А	Ref. IEC 61508-2
Mode of Operation	Low demand operation	
Safety Function, SF1	Valve closing, within specified safety time.	
Safe State, SS1	Valve closed, with specified leakage rate.	
Safety Function, SF2	Valve opening, within specified safety time.	
Safe State, SS2	Valve opened, with specified mass flow rate.	

## **Failure Rates by FMEDA** [failure/10<sup>9</sup> hrs = FIT]

Failure Rate Distribution	$\lambda_{\text{total}}$	$\lambda_{safe}$	$\lambda$ dangerous detected	$\lambda_{dangerous}$ undetected	$\lambda_{don'tcare}$	SFF [%]
SUM (with diagnostic test)	20	0	23	15	61	61
SUM (without diagnostic test)	30	0	0	38	01	0

## Specification of component Architecture

Architecture	1001	is the architecture of a single set of components/component of the analyzed type.
Hardware Fault Tolerance HFT	0	Due to HFT=0, one failure has impact on the safety function of a single set of components/component of the analyzed type.
MTTR / MRT	32 h / 8 h	MTTR is the time required to detect and for repair of the component in case of failure. MRT is the time required for repair of the component. MTTR/MRT has marginal influence on the pfd-value. MRT is exemplary, deviating MRT must be considered in pfd-calculation.
Diagnostic Test	PST	Diagnostic test used to detect dangerous failures during operation. PST: Partial Stroke Test, valves with actuator in open/close application is moved out of activated position. Movement is recognized by a binary sensor (moved / not moved). Valve must leave activated position within a specified time frame. For valves in control applications, position is monitored during control process by continuous comparison of specified and actual valve position.
Diagnostic Coverage (DC)	61 %	In case of missing automatic diagnosis: $DC = 0$ %. In case of implemented diagnostics: $DC > 0$ % (value depends on efficiency of diagnosis). Safe Failure Fraction SFF increased by higher DC.
Diagnostic Test Interval	24 h	Max. diagnostic test interval to perform online diagnostics to detect potential dangerous failures during operation amounts to 24 h. Deviating diagnostic test interval must be considered in pfd- calculation, by deviating MTTR.
Beta Factor	<b>β</b> int <b>= 5%</b> β <sub>Dint</sub> = 2%	Beta factor, which has to be considered if the components/component are used in safety relevant architectures with a HFT ≥ 1. Detailed beta factor has to be calculated for each individual application. The beta factor depends on the exact architecture where the components/component is used in. See IEC 61508-6. table D.5 how to calculate beta factor.

## Verification of SIL Capability (examples considering diagnostic test) (see comments on next page/backside of this page)

Proof Test Interval	1 year	2 years	3 years	4 years	5 years	
<b>PFD</b> avg (IEC 61508-6, B.3.2.2; λ <sub>du</sub> from FME	6.66 E-05	1.32 E-04	1.98 E-04	2.64 E-04	3.29 E-04	
Single component application (H Max. achievable SIL acc. IEC 61508-1, table 2 and IEC 61508-	SIL 2					
Redundant component application Max. achievable SIL acc. IEC 61508-1, table 2 and IEC 61508-	SIL 3					
Calculated (company/name/date/signature)	INGENIEURBÜRO URBAN Anzinger Str. 24 D-85604 Pöring		Pöring, 2022-12	2-22	fortan	

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Explanations to the Data Sheet						
The data sheet is divided in 4 areas:						
• Co	ommon technical description of the set of components/component (blue)					
• Fa • St	<ul> <li>Failure rates (light green)</li> <li>Specification of architecture of the set of components/component (light orange)</li> </ul>					
• Ve	erification of SIL capability (examples) (grey)					
General desc	sription of the Part / Component:					
• Inf	ormation on the set of components/component, type of component and component designator					
• Co	pmponent type (Type A or Type B) acc. IEC 61508-2/7.4.4.1.2 und 7.4.4.1.3)					
• Mo	ode of operation of the set of components/component (acc. IEC 61508-1)					
• De	escription of the safety function of the set of components/component					
Failure Rates	and Failure Rate Distribution					
The failure ra Modes Effect components/ capability of t	tes and failure rate distribution are the results of the reliability calculation of the set of components/ compo is and Diagnostic Analysis (FMEDA). The failure rates can be used for further quantitative analysis of the s component as pfd/pfh-calculation, Markov-Analysis, Fault Tree Analysis, and due to this for a quantitative the set of components/component.	prinent and the Failure set of evaluation of SIL-				
λ <sub>DU</sub> ).	Finally is the distribution the sale range fraction (SFF) is calculated according the formula SFF [ $n$ ] = ( $n$ § :	+ KDD) / (KS + KDD +				
Specification	of Component Architecture					
The architect	ure of the set of components/component is described by following parameters:					
• 50 • Ha	ardware-Fault-Tolerance (HFT) (number of failures acceptable without dispatch on the safety function of th	e set of				
со	mponents/component)					
• Me the da	ean Repair Time (MRT): In case of inspection, the MRT is the mean repair time of the component/set of co e MRT is application specific. The user is responsible to define realistic MRT for the specific application. T tasheet is exemplary, deviating MRT must be considered in pfd-calculation.	omponents. In general, he MRT given in the				
• Me is	ean Time to Repair (MTTR): Mean time to repair the set of components/component in case of detected da the sum of MRT and diagnosis test interval.	ngerous failure. MTTR				
• Di ap gu	agnostic Coverage: The diagnostic coverage is resulting from the diagnostic test for the set of components plication of automatic diagnosis (e.g. partial stroke test). The diagnostic coverage is considered in the FM antitative results of the analysis (see failure rates).	s/component in case of EDA and the				
• Di	agnostic Test: The type of installed on-line automatic diagnostic test to detected dangerous failure during	operation. The				
oia ● Di	agnostic test has to fulfill requirements acc. IEC 61508-2. agnostic Test Interval: Interval between diagnostic tests to detect dangerous failures. Longer diagnostic te	st intervals as				
sp	ecified in the datasheet has to be considered separately in safety parameter calculations, see IEC 61508-	2, 7.4.9.4.				
Be     Co     Sp     ac	<ul> <li>Beta Factor: If the components/component is used in safety relevant architecture with a HFT ≥ 1 a beta factor has to be considered in safety loop calculations. The beta factor for the component is initial (β<sub>int</sub>). To estimate the final beta factor for a specific application the effects of the architecture have to be considered. Thus, the beta factor has to be calculated individual according IEC 6509.6 to the architecture have to be considered. Thus, the beta factor has to be calculated individual according IEC 6509.6 to the architecture have to be considered.</li> </ul>					
• Be	<ul> <li>Beta Factor Diagnostics: β<sub>D</sub> is the fraction of dangerous common cause failures if the components/component is used in safety relevant architectures, which can be detected by diagnostic tests.</li> </ul>					
Se	e IEC 61508-6, table B1.					
The SIL verifi	ication consists of two steps:					
St     Us     IE     St	ep (1) = quantitative verification by calculation of the pfh-value / pfd-value depending from the defined Pro ed architecture. The max. reachable SIL for the calculated safety loop within the component is used can b C 61508-1 table 2 (for low demand operation) or table 3 (for high demand operation) ep (2) = qualitative verification based on the architectural information of the set of components/component	of Test Interval and be estimated according				
according route $1_{H}$ , the qualitative max. SIL is defined in IEC 61508-2, 7.4.4.2.						
for the final s	afety loop not for a single component used in the safety loop.					
IEC 61508-2 permits SIL 3 applications with an architecture with HFT = 0 according to route 1H in case of SFF > 90% for type A components. From technical safety point of view, this can only be accepted if the overall system risk is higher using a redundant safety related architecture in comparison using a single channel architecture. Using non-redundant safety related architectures for SIL 3 application is in general evaluated as insufficient. For SIL 3 application a safety related architecture with HET > 1 is highly recommended						
Further rema	rks using safety relevant parameters					
• If (	operating medium is required (oil, air, etc.), failure rate of operating medium is not considered in the safety	related parameter				
<ul> <li>Failure Rates considering diagnostic measures with DC &gt; 0 may only be used if diagnosis is installed in the application with sufficient quality.</li> </ul>						
• Co sa	Common cause failures, which can occur using the analyzed component in architectures, have to be considered by the user in safety loop calculations					
<ul> <li>If the subsystem is used in application with architectures, e.g. in a 1oo2 architecture, a beta-factor for the subsystem derived from βint acc. IEC 61508-6, table D.5 has to be considered in the safety loop calculation of the application.</li> </ul>						
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